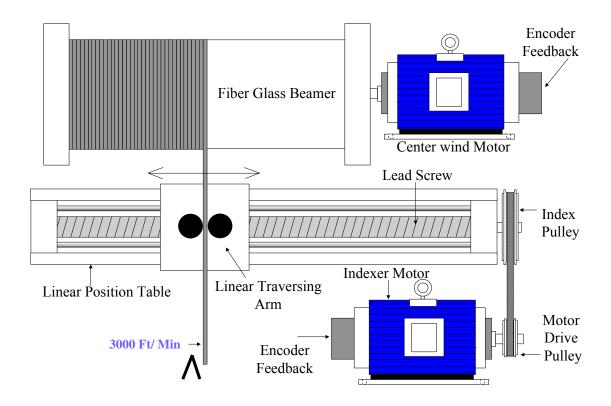


This form is used to help size common indexing applications. The form contains: Indexing overview, sizing example, and customer application data.



Indexing is a method of providing position and velocity control of a machine section or workpiece. Traditionally, Indexer control had been accomplished using stepper and servo controls. With the improvements of Flux Vector AC drives, which regulates the magnetic flux and torque generating current of induction motor, position and velocity control can be accomplished using the less costly Flux Vector drive.

The Servo or Vector drive controls the indexing motion by controlling the motor to move a predefined distance and velocity. An optical encoder or resolver is used to close the position and velocity loop during a move profile. The processor move command will be broken down into a specific number of pulses. During the move command, the encoder pulses provide feedback. By using **CASE** application software, the AC vector drive can count the number of pulses.

The predefined profiles are stored in the software, and the following parameters can be programmed.





Parameters Communication Control

Speed1, Home speed Modbus

Preset Speed 1,2,3 Modbus-Plus

Acceleration RS232-RS485

Deceleration Profibus

Distance Interbus

Dwell

Home sequence

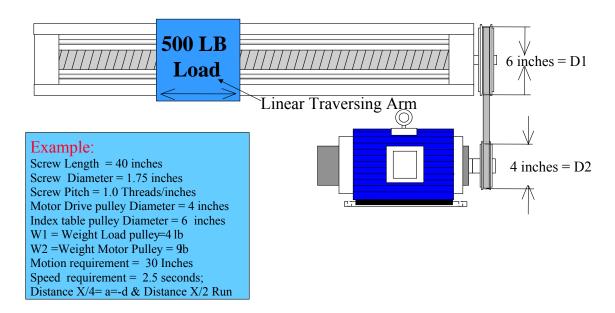
Motion System Performance Comparison

<u>Type</u>	V/f Control	Vector Control	AC Servo
HP Range	0.5-1500 HP	0.5-1500HP	1-100 HP
Speed Range control	40:1	1000:1	200,000:1
Speed control accuracy	± 2%	± .01%	± .01%
Frequency control	1- 400 Hz	1- 400 Hz	1- 400 Hz
Torque Range		.01-150%	.01-200%
Torque Control	No	Yes	Yes
Velocity control	No	Yes	Yes
Positioning	No	Yes	Yes
Repeatability	Not Possible		± 1 arcmin
Motor Inertia:Load Intertia	N/A		10:1-200:1

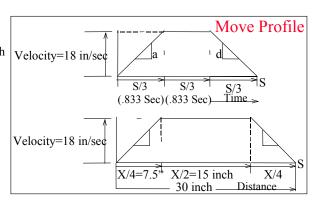


The application below requires calculations that are found on the next page. There are many different sizing programs in the market, but without having the basic understanding of the calculations, a critical profile or mechanical question could be missed.

The calculations require a few assumptions. The velocity & distance profiles are broken up into 3 sections. If you make the assumption that distance is x/4 (x is distance) for acceleration & deceleration, and x/2 for constant velocity, the Time profiles can be broken into s/3 sections (s is time). The profiles are given in the **Move Profile** below.



a = -d = Acceleration =		in/se²
v = Velocity =		in/sec
p = Screw pitch		Threads/Inch
DS = Screw Diameter		inches
W = Load		LBS
F = Breakaway Force		LBS
e = Efficiency of screw		<u> </u>
L=Length of Screw		Inches
J = inertia		oz-in
D1 = Dia Load pulley		inches
D2 = Dia Motor Pulley		inches
W1 = Weight Load pulley	4	lb
W2 =Weight Motor Pulley	9	lb





Formula

Sizing Example

Acceleration = a = -d =
$$\frac{2X}{t^2}$$
 = $\frac{2(X/4)}{(S/3)^2}$ = $\frac{4.5X}{S^2}$

Velocity = at =
$$\frac{4.5X}{S^2} * \frac{S}{3} = \frac{1.5X}{S}$$

Velocity = at =
$$\frac{4.5X}{S^2} * \frac{S}{3} = \frac{1.5X}{S}$$

Torque Friction =
$$\frac{F(D2/D1)}{2\pi *p* e}$$
 & F= Force Friction = $u_s * W$

$$J_{Load @ motor} = \frac{W(D2/D1)^2}{(2\pi p)^2}$$

Steps 1
$$a = -d = \frac{4.5X}{S^2}$$
 $\frac{4.5 * 30}{2.5^2} = 21.6 \text{ in/sec}^2$

②
$$v= at = 1.5 (30 \text{ inch})/2.5 \text{Sec} = 18 \text{ inch} / \text{Sec}$$

$$4$$
 F = Force_{Friction} = .25 * 500 lb * 16 oz/b = 2000 oz

(5) Torque _{Friction} =
$$\frac{(4/6)\ 2000\ \text{oz}}{2\pi*1.0\ \text{threads/in*}.65} = 326\ \text{oz-in}$$

6 J_{Load @ m} =
$$\frac{500 \text{ lb} * 16 \text{ oz/lb} * (4/6)^2}{(2\pi * 1.0 \text{ threads/in})^2} = 90.15 \text{ oz-in}^2$$

$$J_{\; lead\; screw\; @\; motor} = \frac{\pi L \rho R^4 \left(\; D2/D1 \right)^2}{2} \quad ; \; \; \rho = \; Steel\; density = 4.48 \; oz/in^3 \; \bigcirc \ \, J_{\;\; lead\; screw\; @\; m} = \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \; \rho = \; Steel\; density = 4.48 \; oz/in^3 \; \bigcirc \ \, J_{\;\; lead\; screw\; @\; m} = \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \; \rho = \; Steel\; density = 4.48 \; oz/in^3 \; \bigcirc \ \, J_{\;\; lead\; screw\; @\; m} = \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \; \rho = \; Steel\; density = 4.48 \; oz/in^3 \; \bigcirc \ \, J_{\;\; lead\; screw\; @\; m} = \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left(\; 1.75 in/2 \right)^4 \left(\; 4/6 \right)^2}{2} \quad ; \; \sigma = \; \frac{\pi * 40 in * 4.48 oz/in^3 * \left($$

 $Max RPM_{motor} = \frac{Max Speed * Lead Screw Pulley Dia * (60 sec) (3)}{Pitch Dia * Motor Pulley Dia * (min)} RPM_{motor} = \frac{1in/rev *4 in * min}{1in/rev *4 in * min} = 1620 RPM$

 $= 73.29 \text{ oz} - \text{in}^2$

Customer Data

$$J_{load pulley @ motor} = \frac{W_{load Pulley} R^2_{load Pulley} * (D2/D1)^2}{2}$$

$$\omega$$
 $_{@\mbox{ motor}}=$ $2\,\pi^{*}$ p * velocity $_{@\mbox{ t=.833 sec}}$ * (D1/D2)= angular velocity

$$T_{Accel} = \frac{\omega (J_{Load}/e + J_{lead screw} + J_{load pulley} + J_{Motor Pulley} + J_{Motor})}{gt}$$

$$HP = \frac{Torque_{total} * (RPM max)}{5252*12in/lb*12in/ft}$$

(8) J load p @ motor =
$$\frac{9 \text{lb} * 16 \text{ oz} / \text{lb} * 3^2 * (4/6)^2}{2} = 288 \text{ oz-in}^2$$

9
$$J_{\text{Motor Pulley @ motor}} = \frac{6lb * 16 \text{ oz/ lb} * 3^2}{2} = 432 \text{ oz-in}^2$$

(10)
$$\omega_{\text{@motor}} = 2\pi * 1.0 \text{ thread/in * 18 in/sec * (6/4)}$$

$$\frac{\text{(12) T}_{\text{Accel}}}{\text{12 Accel}} = \frac{169.56 (90.15 / .65 + 73.29 + 288 + 432 + 322.56)}{386 \text{in/sec}^2 * .833} = 661 \text{ oz-in}$$

① Torque
$$_{\text{total}}$$
 = (326 oz-in + 661 oz-in) 1.10 = 1085 oz-in



Company Name	☐End user ☐Distributor ☐OEM			
Contact Name #1	Contact Name #1 e-mail			
Contact Name #2	Contact Name #2 e-mail			
Address	City			
State	Zip			
Phone	Fax			

Machine Data

Type of application (Lead Screw, Conveyer, Rack and pinion, Turntable, Machine tool)

Material moved _______

p = Screw pitch ______ Threads/Inch

DS = Screw Diameter ______ inches

W = Load ______ LBS

F = Breakaway Force ______ LBS

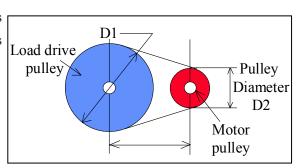
e = Efficiency of screw ______ %

L=Length of Screw ______ Inches

J = inertia ______ oz-in²

Transmission Data, Pulley or chain and sprocket

D1 = Diameter Load pulley or sprocket	 inches
D2 = Diameter Motor Pulley or sprocket	 inches
W1 = Weight Load pulley or sprocket	 lb
W2 =Weight Motor Pulley or sprocket	 _ lb
Inertia of Pulley or sprocket #1 ^A	 oz-in ²
Inertia of Pulley or sprocket #2 ^A	 oz-in ²
Efficiency	 %



^A If not known, then review example above

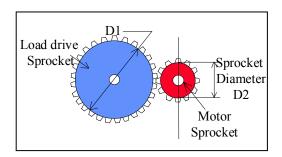


$\boldsymbol{\alpha}$	D	
(<i>tear</i>	K	nν

Gear Box ratio ______ Motor: Load Inertia of Gear Box^B _____ oz-in² Efficiency _____ %

Gears

D1 = Diameter Load Gear inches D2 = Diameter Motor Gear inches Number of teeth Load Gear teeth Number of teeth Motor Gear teeth W1 = Weight Load pulley Gear lb W2 =Weight Motor Gear lb Inertia of Gear^A oz-in² Inertia of Gear^A oz-in² % Efficiency



Move Profile

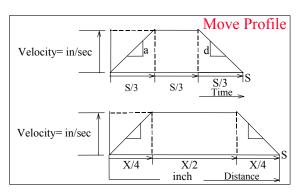
a = -d = Acceleration = _______in/sec² If Acceleration = Deceleration (90% of Applications)

Acceleration = _______in/sec² If Acceleration ≠ Deceleration

Deceleration = _______in/sec² If Acceleration ≠ Deceleration

Machine Design speed _______(Inches/ Seconds)

Minimum move profile ________seconds



^A If not known, then review example above



Indexing Application Report

Drive Data						
Manufacture			Model #			
Horse Power		_				
Winder Drive	☐ New Applic	cation	Retrofit			
Existing Voltage	☐ 230VAC		☐ 460VAC	☐ 575VAC		
Existing Drive system	AC drive	DC drive				
Existing Motor l	Data					
Existing motor Manufac	ture		Model #			
New motor required	Yes	☐ No				
Existing motor full load	ratings:			AMPS		
				Volt		
				RPM (850, 1150, 1750)		
Conduit Box location (į	f motor is to be re	placed)	☐ F1 ☐ F2	☐ F3 or ☐ NA		
Existing Blower Motor.			Voltage	e, Amps or \square NA		
Existing Encoder Manuf	acture			_ _ NA		
Existing Encoder	☐ Digital	l Analog A	C Absolute	Analog DC		
Existing Encoder Manuf	facturer.		NA			
Resolution Existing Enc	oder (PPR)	OR Volts/RPI	М			
Encoder Pickup		Optical	gnetic pickup			
Drive Enclosure	information	1				
Ambient Temperature in	control room		°F or _	°C		
Existing Drive Enclosur	e NEMA 1	☐ NEMA 12	☐ NEMA 4X ☐	AIR CONDITIONING		
New Enclosure Spec	☐ NEMA 1	☐ NEMA 12	☐ NEMA 4X ☐	AIR CONDITIONING		
Enclosure options	Duplex outl	et 🗌 Lights	☐ Empty cabinet f	or future use		
☐ Other						





Existing Power I	Distributio	n				
☐ Isolation Transforme	r KVA	Primary Vo	ltage	AC	Secondary voltage	AC
☐ Line Reactors Imped	Line Reactors Impedence(%) Load Reactors Impedence				(%)	
Dynamic Braking Re	sistor: Duty Cy	cle i.e. 3%, 5	%	%	Resistance	Ohms
Dynamic Resistor Po	wer rating	W	atts			
Drive Communic	cation Rec	uiremen	ts			
☐Modbus Plus ☐Mod	dbus	ce Net \square P	rofibus 🔲 🛚	Arcnet LA	N Other	
Drive Input Req	uirements					
Start	☐ Stop		Forward		Reverse	Run
☐ Jog	☐ Preset Spe	ed1	Preset Spee	ed 2		
Other						
Drive Output Re ☐ Drive alarm fault ☐ At speed ☐ Other	☐ Drive sev	vere fault feedback pass	•		Zero speed	
Analog Input						
speed reference 0)-10VDC	-20ma	Other _			
Analog Output						
☐ Drive Speed (Ft/minute)	☐ Bus Voltag	e	☐ Other			
Special Types of	Control					
☐ Drive system start ☐ DC Bus Over Voltag ☐Other		(Used to prev	ent overvolta	ige tripping	st stop - full current li	-